

Waveguide notes 2010

## Electromagnetic waves in free space

We start with Maxwell's equations in the case that the source terms  $\rho$  and  $\vec{j}$  are both zero.

$$\begin{aligned}\vec{\nabla} \cdot \vec{E} &= 0 & \vec{\nabla} \cdot \vec{B} &= 0 \\ \vec{\nabla} \times \vec{E} &= -\frac{\partial \vec{B}}{\partial t} \\ \vec{\nabla} \times \vec{B} &= \mu_0 \varepsilon_0 \frac{\partial \vec{E}}{\partial t}\end{aligned}$$

Take the curl of Faraday's law:

$$\begin{aligned}\vec{\nabla} \times (\vec{\nabla} \times \vec{E}) &= -\frac{\partial \vec{\nabla} \times \vec{B}}{\partial t} \\ \vec{\nabla} (\vec{\nabla} \cdot \vec{E}) - \nabla^2 \vec{E} &= -\frac{\partial}{\partial t} \mu_0 \varepsilon_0 \frac{\partial \vec{E}}{\partial t}\end{aligned}$$

Use the first Maxwell equation, and we obtain the wave equation with wave speed  $c = 1/\sqrt{\mu_0 \varepsilon_0}$

$$\begin{aligned}\nabla^2 \vec{E} &= \mu_0 \varepsilon_0 \frac{\partial^2 \vec{E}}{\partial t^2} \\ \frac{\partial^2 \vec{E}}{\partial t^2} &= c^2 \nabla^2 \vec{E}\end{aligned}$$

A similar derivation gives the same equation for  $\vec{B}$ . Now let's look at a plane wave solution:

$$\begin{aligned}\vec{E} &= \vec{E}_0 \exp(i\vec{k} \cdot \vec{x} - i\omega t) \\ \vec{B} &= \vec{B}_0 \exp(i\vec{k} \cdot \vec{x} - i\omega t + \phi)\end{aligned}$$

By including the phase constant  $\phi$  in the expression for  $\vec{B}$  we allow for a possible phase shift between  $\vec{E}$  and  $\vec{B}$ . Inserting these into Maxwell's equations, we have

$$\begin{aligned}\vec{\nabla} \cdot \vec{E} &= 0 \Rightarrow \vec{k} \cdot \vec{E}_0 = 0 \\ \vec{\nabla} \cdot \vec{B} &= 0 \Rightarrow \vec{k} \cdot \vec{B}_0 = 0\end{aligned}$$

Thus both  $\vec{E}$  and  $\vec{B}$  are perpendicular to the direction of propagation. From Faraday's law

$$\vec{k} \times \vec{E}_0 \exp(i\vec{k} \cdot \vec{x} - i\omega t) = \omega \vec{B}_0 \exp(i\vec{k} \cdot \vec{x} - i\omega t + \phi)$$

Since this relation must be true for all  $\vec{x}$  and  $t$ , we have  $\phi = 0$  ( $\vec{E}$  and  $\vec{B}$  oscillate in phase) and

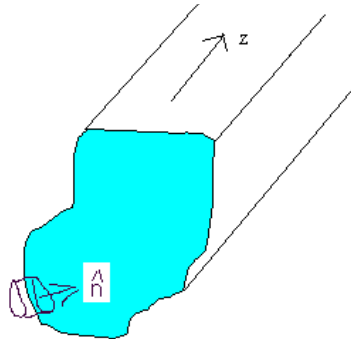
$$\vec{B}_0 = \frac{\vec{k}}{\omega} \times \vec{E}_0 = \frac{1}{c} \hat{k} \times \vec{E}_0$$

Thus  $\vec{B}$  is also perpendicular to  $\vec{E}$ , and its magnitude is  $E/c$ .

If the waves propagate in a LIH material medium, the derivation goes through in the same way using  $\vec{D}$  and  $\vec{H}$ , and the only difference is that the wave speed is  $v = 1/\sqrt{\mu\epsilon} = c/n$ , where the refractive index  $n = \sqrt{\epsilon\mu/\epsilon_0\mu_0}$ .

## Electromagnetic fields in a wave guide

A wave guide is a region with a conducting boundary inside which EM waves are caused to propagate. In this confined region the boundary conditions create constraints on the wave fields. We shall idealize, and assume that the walls are *perfect* conductors. If they are not, currents flowing in the walls lead to energy loss. See Jackson Ch 8 for a discussion of this case.



The boundary conditions at the walls of our perfectly conducting guide are (see notes 1):

$$\hat{n} \cdot \vec{D} = \Sigma \tag{0.1}$$

where  $\Sigma$  is the surface charge density on the wall,

$$\hat{n} \times \vec{E} = 0 \tag{0.2}$$

$$\hat{n} \cdot \vec{B} = 0 \quad (0.3)$$

and

$$\hat{n} \times \vec{H} = \vec{K} \quad (0.4)$$

where  $\vec{K}$  is the surface current density. (Note that we have assumed  $\vec{H} = 0$  inside the conducting material. This is true here because all our fields are assumed to be *time-dependent*, and then non-zero  $\partial\vec{B}/\partial t$  implies nonzero  $\vec{E}$ , by Faraday's law. Non-zero  $\vec{E}$  is not allowed inside a perfect conductor, and so  $\vec{H}$  must be zero too. )

Now we use cylindrical coordinates with  $\hat{z}$  along the guide in the direction of wave propagation. The transverse coordinates will be chosen to match the cross-sectional shape of the guide – Cartesian for a rectangular guide and polar for a circular guide. Next we assume that all fields may be written in the form

$$\vec{E} = \vec{E}_0(\vec{x}) e^{-i\omega t}$$

We are not making any special assumptions about the time variation, because we can always Fourier transform the fields to get combinations of terms of this form. Then Maxwell's equations in the guide take the form:

$$\begin{aligned} \vec{\nabla} \times \vec{E} &= i\omega\vec{B} \\ \vec{\nabla} \cdot \vec{D} &= 0 \quad \vec{\nabla} \cdot \vec{B} = 0 \end{aligned}$$

and

$$\vec{\nabla} \times \vec{H} = -i\omega\vec{D}$$

Taking the curl of Faraday's law, and inserting  $\vec{\nabla} \times \vec{B}$  from Ampere's law, we get:

$$\begin{aligned} \vec{\nabla} \times (\vec{\nabla} \times \vec{E}) &= \vec{\nabla} (\vec{\nabla} \cdot \vec{E}) - \nabla^2 \vec{E} = i\omega\vec{\nabla} \times \vec{B} = i\omega \left( -i\frac{\omega}{c^2} \mu\epsilon \vec{E} \right) \\ \nabla^2 \vec{E} &= -\omega^2 \mu\epsilon \vec{E} \end{aligned} \quad (0.5)$$

This equation is the same as we obtained for free space.

Next we look for solutions that take the form of waves propagating in the  $z$ -direction, that is:

$$\vec{E}_0(\vec{x}) = \vec{E}_a(x, y) e^{ikz}$$

The wave equation (0.5) then becomes:

$$\nabla_{\perp}^2 \vec{E} + \omega^2 \mu\epsilon \vec{E} - k^2 \vec{E} = 0 \quad (0.6)$$

where  $\nabla_t^2$  is the Laplacian operator in the two transverse coordinates ( $x$  and  $y$ , or  $\rho$  and  $\phi$ , for example.) Thus equation (0.6) is an equation for the function  $\vec{E}_a$  of the two transverse coordinates.

Since we were able to simplify the equations by separating the function  $\vec{E}$  into its dependence on the coordinates along and transverse to the guide, we now try to do the same thing with the components. At first glance you might want to jump to the conclusion that there is no  $z$ -component of a wave propagating in the  $z$ -direction, but in general there is. The waves are propagating between conducting boundaries, and we have to allow for the possibility that waves travel at an angle to the guide center-line, and bounce back and forth off the walls as they travel. Since  $\vec{E}$  is perpendicular to the wave vector,  $\vec{E}$  in such a bouncing wave has a  $z$ -component. The total electromagnetic disturbance in the guide is a sum of such waves. The sum is a combination of waves that interfere constructively. Thus

$$\vec{E}_a = E_z \hat{z} + \vec{E}_t$$

and similarly

$$\vec{B}_a = B_z \hat{z} + \vec{B}_t$$

This decomposition simplifies the boundary conditions, since  $\hat{n}$  has no  $z$ -component. Thus equation (0.2) has two components. The transverse component gives

$$E_z = 0 \text{ on } S \tag{0.7}$$

while the  $z$ - component gives

$$\hat{n} \times \vec{E}_t = 0 \text{ on } S \tag{0.8}$$

and eqn (0.3) becomes

$$\hat{n} \cdot \vec{B}_t = 0 \text{ on } S \tag{0.9}$$

Next we separate Maxwell's equations into components too. The "divergence" equations are easiest, so let's start with them:

$$\vec{\nabla} \cdot \vec{D} = 0 = \varepsilon \left( \frac{\partial E_z}{\partial z} + \vec{\nabla}_t \cdot \vec{E}_t \right)$$

and evaluating the  $z$ -derivative, we get

$$ikE_z + \vec{\nabla}_t \cdot \vec{E}_t = 0 \tag{0.10}$$

Similarly:

$$ikB_z + \vec{\nabla}_t \cdot \vec{B}_t = 0 \quad (0.11)$$

For the curl equations, we take the dot product with  $\hat{z}$ :

$$\hat{z} \cdot (\vec{\nabla} \times \vec{E}) = i\omega B_z = \hat{z} \cdot (\vec{\nabla}_t \times \vec{E}_t) \quad (0.12)$$

and also the cross product:

$$\hat{z} \times (\vec{\nabla} \times \vec{E}) = \hat{z} \times i\omega \vec{B}$$

Let's investigate the triple cross product on the left. Since  $\hat{z}$  is a constant we may move it through the  $\nabla$  operator:

$$\hat{z} \times (\vec{\nabla} \times \vec{E}) = \vec{\nabla} (\hat{z} \cdot \vec{E}) - (\hat{z} \cdot \vec{\nabla}) \vec{E}$$

The derivative  $\partial E_z / \partial z$  times  $\hat{z}$  appears in both terms, and so cancels, leaving:

$$\vec{\nabla}_t E_z - \frac{\partial}{\partial z} \vec{E}_t = i\omega \hat{z} \times \vec{B}_t$$

Thus

$$\vec{\nabla}_t E_z - ik\vec{E}_t = i\omega \hat{z} \times \vec{B}_t \quad (0.13)$$

and similarly from Ampere's law we have:

$$\vec{\nabla}_t B_z - ik\vec{B}_t = -i\omega \epsilon \mu \hat{z} \times \vec{E}_t \quad (0.14)$$

and

$$-i\omega \epsilon \mu E_z = \hat{z} \cdot (\vec{\nabla}_t \times \vec{B}_t) \quad (0.15)$$

Equations (0.10), (0.11), (0.15) and (0.12) show that the longitudinal components  $E_z$  and  $B_z$  act as sources of the transverse fields  $\vec{B}_t$  and  $\vec{E}_t$ .

Now we can simplify by looking at two sets of normal modes:

**Transverse Electric** (or magnetic) **modes.**

In these modes there is no longitudinal component of  $\vec{E}$ :

$$E_z \equiv 0 \text{ everywhere}$$

Thus boundary condition (0.7) is automatically satisfied. The remaining boundary condition is (0.9), and we can find the version that we need by taking the dot product of  $\hat{n}$  with equation (0.14):

$$-ik\hat{n} \cdot \vec{B}_t + \hat{n} \cdot \vec{\nabla}_t B_z = -i\omega\varepsilon\mu\hat{n} \cdot (\hat{z} \times \vec{E}_t)$$

The first term is zero on  $S$ , and we rearrange the triple scalar product on the right, leaving:

$$\frac{\partial B_z}{\partial n} = i\omega\varepsilon\mu\hat{z} \cdot (\hat{n} \times \vec{E}_t) = 0 \text{ on } S \quad (0.16)$$

where we used the other boundary condition (0.8) for  $\vec{E}$ .

**Transverse Magnetic** (or electric) **modes.**

In these modes there is no longitudinal component of  $\vec{B}$ :

$$B_z \equiv 0 \text{ everywhere}$$

Thus the boundary condition (0.16) is trivially satisfied, and we must impose the remaining condition (0.7)

$$E_z = 0 \text{ on } S.$$

Since the Maxwell equations are linear, we can form superpositions of these two sets of modes to obtain fields in the guide with non-zero longitudinal components of both  $\vec{E}$  and  $\vec{B}$ . These modes are the result of the constructive interference mentioned above.

Now let's see how the equations simplify.

**TM modes**

We start by finding an equation for  $E_z$ . Equation (0.14) simplifies to:

$$\begin{aligned} -ik\vec{B}_t &= -i\omega\varepsilon\mu\hat{z} \times \vec{E}_t \\ \vec{B}_t &= \frac{\omega}{k}\varepsilon\mu\hat{z} \times \vec{E}_t \end{aligned} \quad (0.17)$$

and we substitute this result back into equation (0.13).

$$\begin{aligned} -ik\vec{E}_t + \vec{\nabla}_t E_z &= i\omega\hat{z} \times \left( \frac{\omega}{k}\varepsilon\mu\hat{z} \times \vec{E}_t \right) \\ \vec{\nabla}_t E_z &= ik\vec{E}_t - i\frac{\omega^2}{k}\varepsilon\mu\vec{E}_t \\ &= ik \left( 1 - \frac{\omega^2}{k^2}\varepsilon\mu \right) \vec{E}_t \end{aligned} \quad (0.18)$$

and finally we substitute this result back into equation (0.10):

$$\begin{aligned} ikE_z + \vec{\nabla}_t \cdot \frac{\vec{\nabla}_t E_z}{ik \left(1 - \frac{\omega^2}{k^2} \varepsilon \mu\right)} &= 0 \\ \nabla_t^2 E_z + (\omega^2 \varepsilon \mu - k^2) E_z &= 0 \end{aligned}$$

or

$$\nabla_t^2 E_z + \gamma^2 E_z = 0 \quad (0.19)$$

with

$$\gamma^2 \equiv \omega^2 \varepsilon \mu - k^2 \quad (0.20)$$

Equation (0.19) is the defining differential equation for  $E_z$ . Once we have solved for  $E_z$ , we can find  $\vec{E}_t$  from equation (0.18) and then  $\vec{B}_t$  from equation (0.17).

### **TE modes**

The argument proceeds similarly. We start with equation (0.13), to get:

$$\vec{E}_t = -\frac{\omega}{k} \hat{z} \times \vec{B}_t \quad (0.21)$$

Then use equation (0.14)

$$\begin{aligned} -ik\vec{B}_t + \vec{\nabla}_t B_z &= -i\omega\varepsilon\mu\hat{z} \times \left(-\frac{\omega}{k}\hat{z} \times \vec{B}_t\right) \\ \vec{\nabla}_t B_z &= i \left(k - \frac{\omega^2 \varepsilon \mu}{k}\right) \vec{B}_t \end{aligned} \quad (0.22)$$

and finally from equation (0.11) we have:

$$\begin{aligned} ikB_z + \vec{\nabla}_t \cdot \frac{\vec{\nabla}_t B_z}{i \left(k - \frac{\omega^2 \varepsilon \mu}{k}\right)} &= 0 \\ \nabla_t^2 B_z + \gamma^2 B_z &= 0 \end{aligned}$$

which is the same differential equation that we found for  $E_z$  in the TM modes. The solutions are different because the boundary conditions are different. Thus the solution for the two modes proceeds as follows:

	<b>TM modes</b>	<b>TE modes</b>
assumed	$B_z = 0$	$E_z = 0$
differential equation	$\nabla_t^2 E_z + \gamma^2 E_z = 0$	$\nabla_t^2 B_z + \gamma^2 B_z = 0$
boundary condition	$E_z = 0$ on S	$\frac{\partial B_z}{\partial n} = 0$ on S
next find	$\vec{E}_t = \frac{ik}{\gamma^2} \vec{\nabla}_t E_z$	$\vec{B}_t = \frac{ik}{\gamma^2} \vec{\nabla}_t B_z$
then find	$\vec{B}_t = \frac{\omega}{k} \varepsilon \mu \hat{z} \times \vec{E}_t$	$\vec{E}_t = -\frac{\omega}{k} \hat{z} \times \vec{B}_t$

The differential equation plus boundary condition is an eigenvalue problem that produces a set of eigenfunctions  $E_z$  (or  $B_z$ ) and a set of eigenvalues  $\gamma_n$ . The wave number  $k$  is then determined from equation (0.20):

$$k_n^2 = \omega^2 \varepsilon \mu - \gamma_n^2 \quad (0.23)$$

Clearly if  $\gamma_n$  is greater than  $\omega \sqrt{\varepsilon \mu} = \omega/v$ , where  $v$  is the wave speed,  $k$  becomes imaginary and the wave does not propagate. There is a cut-off frequency for each mode, given by

$$\omega_n = \gamma_n v$$

If  $\gamma_1$  is the *lowest* eigenvalue, the corresponding frequency  $\omega_1$  is *the* cutoff frequency for the guide, and waves at lower frequencies cannot propagate.

A few things to note: the wave number  $k_n$  is always less than the free-space value  $\omega/v$ , and thus the wavelength is always greater than the free-space wavelength. The phase speed is

$$v_\phi = \frac{\omega}{k} = \frac{1}{\sqrt{\mu \varepsilon}} \frac{1}{\sqrt{1 - \omega_n^2/\omega^2}} > \frac{1}{\sqrt{\mu \varepsilon}}$$

and we can differentiate eqn (0.23) to get

$$2\omega \frac{d\omega}{dk} \varepsilon \mu = 2k$$

Then the group speed is

$$v_g = \frac{d\omega}{dk} = \frac{2k}{2\omega \varepsilon \mu} = \frac{1}{\mu \varepsilon v_\phi} = \frac{1}{\sqrt{\mu \varepsilon}} \sqrt{1 - \frac{\omega_n^2}{\omega^2}} < \frac{1}{\sqrt{\mu \varepsilon}}$$

Thus information travels more slowly than if the wave were to propagate in free space.

## TM modes in a rectangular wave guide

Let the guide have dimensions  $a$  in the  $x$ -direction by  $b$  in the  $y$ -direction. Let the interior be full of air so  $\varepsilon/\varepsilon_0 = \mu/\mu_0 = 1$ . Then the differential equation for  $E_z$  is

$$\left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \gamma^2 \right) E_z = 0$$

As usual we look for a separated solution, choosing  $E_z = X(x)Y(y)$  to obtain:

$$\frac{X''}{X} + \frac{Y''}{Y} + \gamma^2 = 0$$

Each term must separately be constant, so we have:

$$\frac{X''}{X} = -\alpha^2$$

$$\frac{Y''}{Y} = -\beta^2$$

and

$$-\alpha^2 - \beta^2 + \gamma^2 = 0$$

The boundary conditions are:

$$X = 0 \text{ at } x = 0 \text{ and } x = a$$

and

$$Y = 0 \text{ at } y = 0 \text{ and } y = b$$

Thus the appropriate solutions are  $X = \sin \alpha x$  and  $Y = \sin \beta y$  with eigenvalues chosen to fit the second boundary condition in each coordinate:

$$\alpha = \frac{n\pi}{a} \text{ and } \beta = \frac{m\pi}{b}$$

Thus

$$E_z = E_0 \sin \frac{n\pi x}{a} \sin \frac{m\pi y}{b} e^{ikz - i\omega t}$$

and

$$\gamma_{nm}^2 = \left( \frac{n\pi}{a} \right)^2 + \left( \frac{m\pi}{b} \right)^2$$

Notice that the lowest possible values of  $n$  and  $m$  are 1 in each case, since taking  $m$  or  $n = 0$  would render  $E_z$  identically zero. Thus the lowest eigenvalue is

$$\gamma_{11} = \pi \sqrt{\frac{1}{a^2} + \frac{1}{b^2}}$$

and the cutoff frequency for the TM modes is:

$$\omega_{c,\text{TM}} = c\gamma_{11} = c\pi \sqrt{\frac{1}{a^2} + \frac{1}{b^2}}$$

Jackson solves for the TE modes (pg 361). The eigenvalues are the same, but in this case it is possible for one (but not both) of  $m$  and  $n$  to be zero, leading to a lower cutoff frequency:

$$\omega_{c,\text{TE}} = \frac{c\pi}{a}$$

assuming  $a > b$ . This would be *the* cutoff frequency for the guide.

In the TM mode, the remaining fields are:

$$\begin{aligned} \vec{E}_t &= \frac{ik}{\gamma^2} \vec{\nabla}_t E_0 \sin \frac{n\pi x}{a} \sin \frac{m\pi y}{b} e^{ikz-i\omega t} \\ &= \frac{ik}{\gamma^2} E_0 \left( \frac{n\pi}{a} \hat{x} \cos \frac{n\pi x}{a} \sin \frac{m\pi y}{b} + \frac{m\pi}{b} \hat{y} \sin \frac{n\pi x}{a} \cos \frac{m\pi y}{b} \right) e^{ikz-i\omega t} \end{aligned}$$

and

$$\begin{aligned} \vec{B}_t &= \frac{\omega}{kc^2} \hat{z} \times \frac{ik}{\gamma^2} E_0 \left( \frac{n\pi}{a} \hat{x} \cos \frac{n\pi x}{a} \sin \frac{m\pi y}{b} + \frac{m\pi}{b} \hat{y} \sin \frac{n\pi x}{a} \cos \frac{m\pi y}{b} \right) e^{ikz-i\omega t} \\ &= i \frac{\omega}{c^2 \gamma^2} E_0 \left( \frac{n\pi}{a} \hat{y} \cos \frac{n\pi x}{a} \sin \frac{m\pi y}{b} - \frac{m\pi}{b} \hat{x} \sin \frac{n\pi x}{a} \cos \frac{m\pi y}{b} \right) e^{ikz-i\omega t} \end{aligned}$$

As usual the physical fields are given by the real part of each mathematical expression. You should verify that these fields satisfy the boundary conditions at  $x = 0, a$  and at  $y = 0, b$ .

## Power

The power transmitted in the guide is:

$$\vec{S}(t) = \frac{1}{\mu_0} \vec{E} \times \vec{B}$$

where here we must take the real, physical fields. Usually we are interested in the time-averaged Poynting flux

$$\langle \vec{S} \rangle = \text{Re} \frac{1}{2\mu_0} \vec{E} \times \vec{B}^*$$

where the fields on the right are the complex functions we have just found.

**Proof** of this result:

If  $\vec{E} = \vec{E}_0 e^{-i\omega t} = \hat{e} E_0 e^{i\phi} e^{-i\omega t}$  and similarly for  $\vec{B}$ , then:

$$\begin{aligned} \langle \vec{S} \rangle &= \langle \hat{e} \times \hat{b} \frac{E_0 B_0}{\mu_0} \cos^2(\phi - \omega t) \rangle \\ &= \langle \hat{e} \times \hat{b} \frac{E_0 B_0}{\mu_0} (\cos \phi \cos \omega t + \sin \phi \sin \omega t)^2 \rangle \\ &= \langle \hat{e} \times \hat{b} \frac{E_0 B_0}{\mu_0} (\cos^2 \phi \cos^2 \omega t + 2 \cos \phi \cos \omega t \sin \phi \sin \omega t + \sin^2 \phi \sin^2 \omega t) \rangle \\ &= \hat{e} \times \hat{b} \frac{E_0 B_0}{2\mu_0} (\cos^2 \phi + \sin^2 \phi) = \hat{e} \times \hat{b} \frac{E_0 B_0}{2\mu_0} \end{aligned}$$

and

$$\frac{1}{2\mu_0} \vec{E} \times \vec{B}^* = \hat{e} \times \hat{b} \frac{E_0 B_0}{2\mu_0}$$

so the two results are the same. (Be sure that you understand why  $\vec{E}$  and  $\vec{B}$  are in phase.)

Using our solution, the components are:

$$\begin{aligned} \langle S_z \rangle &= \text{Re} \frac{1}{2\mu_0} (E_x B_y^* - E_y B_x^*) \\ &= \text{Re} \frac{1}{2\mu_0} \frac{ik}{\gamma^2} E_0 (-i) \frac{\omega}{c^2 \gamma^2} E_0 \left[ \left( \frac{n\pi}{a} \cos \frac{n\pi x}{a} \sin \frac{m\pi y}{b} \right)^2 + \left( \frac{m\pi}{b} \sin \frac{n\pi x}{a} \cos \frac{m\pi y}{b} \right)^2 \right] \\ &= \frac{E_0^2}{2\mu_0} \frac{k}{\gamma^4} \frac{\omega}{c^2} \left[ \left( \frac{n\pi}{a} \cos \frac{n\pi x}{a} \sin \frac{m\pi y}{b} \right)^2 + \left( \frac{m\pi}{b} \sin \frac{n\pi x}{a} \cos \frac{m\pi y}{b} \right)^2 \right] \\ &= \frac{E_0^2}{2\mu_0} \frac{\sqrt{\omega^2/c^2 - \gamma^2}}{\gamma^4} \frac{\omega}{c^2} \left[ \left( \frac{n\pi}{a} \cos \frac{n\pi x}{a} \sin \frac{m\pi y}{b} \right)^2 + \left( \frac{m\pi}{b} \sin \frac{n\pi x}{a} \cos \frac{m\pi y}{b} \right)^2 \right] \\ &= \frac{E_0^2}{2\mu_0} \frac{\sqrt{\frac{\omega^2}{c^2} - \left(\frac{n\pi}{a}\right)^2 - \left(\frac{m\pi}{b}\right)^2}}{\left[\left(\frac{n\pi}{a}\right)^2 + \left(\frac{m\pi}{b}\right)^2\right]^2} \frac{\omega}{c^2} \left[ \left( \frac{n\pi}{a} \cos \frac{n\pi x}{a} \sin \frac{m\pi y}{b} \right)^2 + \left( \frac{m\pi}{b} \sin \frac{n\pi x}{a} \cos \frac{m\pi y}{b} \right)^2 \right] \end{aligned}$$

$\langle S_z \rangle$  is positive for all values of  $x$  and  $y$ , showing that power is propagating continuously along the guide in the positive  $z$ -direction.

The transverse component  $S_x$  is:

$$\begin{aligned} \langle S_x \rangle &= \operatorname{Re} \frac{1}{2\mu_0} (E_y B_z^* - E_z B_y^*) = \operatorname{Re} \frac{1}{2\mu_0} (-E_z B_y^*) \\ &= \operatorname{Re} \frac{1}{2\mu_0} \left( -E_0 \sin \frac{n\pi x}{a} \sin \frac{m\pi y}{b} (-i) \frac{\omega}{c^2 \gamma^2} E_0 \frac{n\pi}{a} \cos \frac{n\pi x}{a} \sin \frac{m\pi y}{b} \right) \\ &= 0 \end{aligned}$$

Because there is no real part, the time averaged power flowing across the guide is zero. Power sloshes back and forth, but there is no net energy transfer.

## Fields in a parallel plate wave guide

By simplifying the shape of the guide even more, we can demonstrate how the wave modes are formed by reflection of waves at the guide walls. Let this guide exist in the region  $0 \leq y \leq a$ . For the TM mode, the equation to be satisfied is:

$$(\nabla_t^2 + \gamma^2) E_z = 0$$

with

$$E_z = 0 \text{ at } y = 0 \text{ and } y = a$$

Because the region is infinite in the  $x$ -direction, the appropriate solution has no  $x$ -dependence:

$$E_z = E_0 \sin \frac{n\pi y}{a} e^{ikz - i\omega t}$$

with

$$\gamma_n = \frac{n\pi}{a}$$

Thus the cutoff frequency for this mode is

$$\omega_c = \gamma_1 c = \frac{\pi c}{a}$$

Then the other components of the fields are:

$$\begin{aligned} \vec{E}_t &= \frac{ik}{\gamma^2} \vec{\nabla}_t E_z = \frac{ik}{\gamma^2} \frac{n\pi}{a} E_0 \cos \frac{n\pi y}{a} e^{ikz - i\omega t} \hat{y} \\ &= \frac{ika}{n\pi} E_0 \cos \frac{n\pi y}{a} e^{ikz - i\omega t} \hat{y} \end{aligned}$$

and

$$\begin{aligned}\vec{B}_t &= \frac{\omega}{kc^2} \hat{z} \times \vec{E}_t = -\frac{\omega}{kc^2} \frac{ika}{n\pi} E_0 \cos \frac{n\pi y}{a} e^{ikz-i\omega t} \hat{x} \\ &= -\frac{\omega}{c^2} \frac{ia}{n\pi} E_0 \cos \frac{n\pi y}{a} e^{ikz-i\omega t} \hat{x}\end{aligned}\quad (0.24)$$

Let's look at the electric fields first. We write the sine and cosine as combinations of complex exponentials:

$$E_z = E_0 \left( \frac{e^{i\gamma y} - e^{-i\gamma y}}{2i} \right) e^{ikz-i\omega t} = i \frac{\gamma}{\gamma} E_0 \left( \frac{e^{-i\gamma y} - e^{i\gamma y}}{2} \right) e^{ikz-i\omega t}$$

and

$$E_y = \frac{ik}{\gamma} E_0 \left( \frac{e^{i\gamma y} + e^{-i\gamma y}}{2} \right) e^{ikz-i\omega t}$$

Thus we can write the electric field as a superposition

$$\vec{E} = \frac{1}{2} (\vec{E}_1 + \vec{E}_2)$$

where the two superposed fields are

$$\vec{E}_1 = i(k\hat{y} - \gamma\hat{z}) \frac{E_0}{\gamma} \exp(ikz + i\gamma y) e^{-i\omega t}$$

and

$$\vec{E}_2 = i(k\hat{y} + \gamma\hat{z}) \frac{E_0}{\gamma} \exp(ikz - i\gamma y) e^{-i\omega t}$$

Similarly:

$$\vec{B}_t = -i \frac{\omega}{c^2 \gamma} E_0 \hat{x} \left( \frac{e^{i\gamma y} + e^{-i\gamma y}}{2} \right) e^{ikz-i\omega t} = \frac{1}{2} (\vec{B}_1 + \vec{B}_2)$$

with

$$\vec{B}_{1,2} = -i \frac{\omega}{\gamma c^2} E_0 \hat{x} \exp[i(kz \pm \gamma y)]$$

Now define the four vectors

$$\vec{u}_1 = k\hat{y} - \gamma\hat{z}; \quad \vec{u}_2 = k\hat{y} + \gamma\hat{z}$$

and

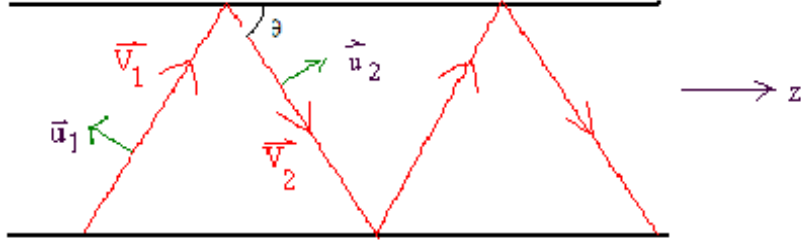
$$\vec{v}_1 = k\hat{z} + \gamma\hat{y}; \quad \vec{v}_2 = k\hat{z} - \gamma\hat{y}$$

Then for  $i = 1, 2$

$$\vec{u}_i \cdot \vec{v}_i = 0$$

and

$$\vec{v}_1 \times \vec{u}_1 = (k\hat{z} + \gamma\hat{y}) \times (k\hat{y} - \gamma\hat{z}) = -\hat{x}(\gamma^2 + k^2) = -\hat{x}\frac{\omega^2}{c^2}$$



The two electric field components are then:

$$\vec{E}_1 = i\vec{u}_1 \frac{E_0}{\gamma} \exp(i\vec{v}_1 \cdot \vec{x}) e^{-i\omega t} \quad \text{and} \quad \vec{E}_2 = i\vec{u}_2 \frac{E_0}{\gamma} \exp(i\vec{v}_2 \cdot \vec{x}) e^{-i\omega t}$$

while

$$\frac{\vec{v}_1 \times \vec{E}_1}{\omega} = \vec{B}_1 = -i\frac{\omega}{\gamma c^2} \hat{x} E_0 \exp[i(kz + \gamma y)]$$

consistent with (0.24)

Each of these sets of fields ( $\vec{E}_1$  and  $\vec{B}_1$ ,  $\vec{E}_2$  and  $\vec{B}_2$ ) has the form of a free-space wave propagating in the direction given by the vectors  $\vec{v}_1$  and  $\vec{v}_2$  respectively and with wave number

$$|\vec{v}_1| = |\vec{v}_2| = \sqrt{\gamma^2 + k^2} = \frac{\omega}{c}$$

. These waves are moving across the guide at an angle given by

$$\tan \theta = \frac{v_y}{v_z} = \pm \frac{\gamma}{k} = \pm \frac{\gamma}{\sqrt{\frac{\omega^2}{c^2} - \gamma^2}}$$

that is, the waves are reflecting off the plates at  $y = 0, a$ . When the angle  $\theta$  becomes  $\pi/2$ , the wave ceases to propagate along the guide, but just bounces back and forth. This happens when  $\tan \theta \rightarrow \infty$ , or

$$\gamma = \frac{\omega}{c}$$

This gives the cut-off frequency we found before.